

## #2.1

	psf
Hardwood	4
Plywood	3
Framing	2.6
Ceiling supports	0.5
Gypsum wallboard	5
Total	15.1

## #2.2

1. Concrete slab/unit area	
1 ft x 1ft x 1/12 ft x 150 pcf	12.5
2. Framing DL adjustment	
<u>Load @ 4 in. OC, i.e 3 sect/ft</u>	2.6
Load/section	$2.6/3$
At 3 in. OC, # sections/ft	4
Load of 4 sec/ft @ 3 in OC	$4 * 2.6/3 =$ 3.47

## 3. Floor DL

Concrete slab	12.5
Plywood	3
Framing	3.47
Ceiling supports	0.5
Gypsum wallboard	5
Total	24.47

## #2.3

1. $L_0$ , psf	40
2. Tributary area = 20 x 17.5	350
3. For interior beam, $K_{LL}$	2
4. $K_{LL}A_T = 2 * 350$	700
5. $K = 0.25 + \frac{15}{\sqrt{700}}$	0.82
$LL = k L_0 = 0.82 * 40$	32.68

## # 2.4

1. Basic LL for office	50
2. $A_T = 40 * 40$	1600
3. For interior column $K_{LL}$	4
4. $K_{LL}A_T$	6400
5. $K = 0.25 + \frac{15}{\sqrt{6400}}$	0.44 Use min 0.5
$LL = 50 * 0.5$	250

## # 2.5

1. For gymnasium $L_o$ , psf	100.00	
2. $A_T = 50 \times 20$	1000.00	
3. $K_{LL}$	4.00	
4. $K_{LL}A_T$	4000.00	
5. $K = 0.25 + \frac{15}{\sqrt{4000}}$	0.49 Use min	0.50
$LL = 100 \times 0.5$	50.00	

## # 2.6

1. $K_{LL}$	1.00	
2. $A_T = 50 \times 20$	1000.00	
4. $K_{LL}A_T$	1000.00	
5. $K = 0.25 + \frac{15}{\sqrt{1000}}$	0.72	
$LL = 100 \times 0.72$	72.00	

## # 2.7

1. Office from 2 floors $L_o$ , psf	100.00	
2. $A_T = 40 \times 40$	1600.00	
3. $K_{LL}$	4.00	
4. $K_{LL}A_T$	6400.00	
5. $K = 0.25 + \frac{15}{\sqrt{6400}}$	0.44 > 0.4 for two floors	
6. $LL = 100 \times 0.44$	44.00	
7. Alternative LL		
$0.7(L_1 + L_2 + L_3 + \dots) = 0.7 \times 100$	70.00 ← Controls	

## # 2.8

1. Total load = $30 + 25 + 20$ , psf	75.00	
2. $A_T = 25 \times 30$	750.00	
3. $K_{LL}$	2.00	
4. $K_{LL}A_T$	1500.00	
5. $K = 0.25 + \frac{15}{\sqrt{1500}}$	0.64	
6. $LL = 75 \times 0.64$	48.00	
7. Alternative LL		
$0.7(L_1 + L_2 + L_3 + \dots)$		
$0.7(30 + 25 + 20)$	52.50 ← Controls	
8. Min LL = Max on a floor = 30		

### # 2.9

1.  $LL = L (1 + IF)$
2.  $IF = 1$  for Elevator  
     $= 0.33$  for Hanger                      1.33
3.  $LL = 52.5 (1 + 1.33)$                       122.325

### # 2.10

1. For gymnasium  $L_o$ , psf                      100.00
2.  $A_T = 50 \times 20$                       1000.00
3. For interior beam  $K_{LL}$                       2.00
4.  $K_{LL} A_T$                       2000.00
5.  $K = 0.25 + \frac{15}{\sqrt{2000}}$                       0.585
6.  $LL = 100 \times 0.585$                       58.54
7. Design Load  
    LL                      58.54  
    Impact factor 50%                      29.27  
    Partition load                      15.00
- Total                      102.81

### # 2.11

1. Roof live load  $L_o$ , psf                      20.00
2. Roof angle  $\theta = \tan^{-1} (6.3/10)$                       32.23
3. Horizontal dist =  $W \cos \theta$                       20.31
4.  $A_T = 10 \times 20.31$                       203.10
5.  $R_1 = 1.2 - 0.001 \times A_T$                       1.00
6.  $R_2 = 1.2 - 0.6 \times \tan \theta$                       0.82
7.  $L_r = R_1 \times R_2 \times L_o$                       16.39

### # 2.12

1. Roof live load  $L_o$ , psf                      20.00
2. Roof angle  $\theta = \tan^{-1} (6.3/10)$                       32.23
3. Horizontal dist =  $W \cos \theta$                       20.31
4.  $A_T = 4 \times 20.31$                       81.22  $< 200 \text{ ft}^2$        $R_1 = 1$
5. Since  $A_T < 200$   $R_1 = 1$                       1.00
6.  $R_2 = 1.2 - 0.6 \times \tan \theta$                       0.82
7.  $L_r = R_1 \times R_2 \times L_o$                       16.44

## # 2.13

1. Roof live load $L_0$ , psf	20	
2. Roof angle $\theta = \tan^{-1}(1/2)$	26.57	
3. Horizontal dist = W	15	
4. $A_T = 15 \times 40$	600	
5. $R_1 = 1.2 - 0.001 \times A_T$	0.6	
6. $R_2 = 1.2 - 0.6 \times \tan \theta$	0.90	
7. $L_r = R_1 \times R_2 \times L_0$	10.80 < 12 psf	Use 12
8. Minimum roof live load	12.00 psf	

## # 2.14

1. Roof live load $L_0$ , psf	20.00
2. Roof angle $\theta = \tan^{-1}(1/2)$	26.57
3. Horizontal wall dist = W	7.50
4. $A_T = 7.5 \times 40$	300.00
5. $R_1 = 1.2 - 0.001 \times A_T$	0.90
6. $R_2 = 1.2 - 0.6 \times \tan \theta$	0.90
7. $L_r = R_1 \times R_2 \times L_0$	16.20

## # 2.15

Special roof live load are not reduced by roof live load reductions  $R_1$  and  $R_2$ . However, these will be reduced by the provisions of floor live loads

1. For garden roof $L_0$ , psf	100.00
2. $A_T = 250$	250.00
3. $K_{LL}$	4.00
4. $K_{LL} A_T$	1000.00
5. $K = 0.25 + \frac{15}{\sqrt{1000}}$	0.724
$L_r = 100 \times 0.72$	72.43